

On a model of flows in a deformable porous solid with small strain and density depending material modulus

V. Girault

Laboratoire Jacques-Louis Lions, Sorbonne Université, Paris 6
Workshop on PDEs and Control 2025 (PKM-60)

Common work with

A. Bonito, Texas A & M University,
D. Guignard, University of Ottawa,
K.R. Rajagopal, Texas A & M University

PKM-60

Outline

1 The model

2 An attempt at analysis

3 Discretization

The model

MODEL

Introducing the model

- The model I shall present was proposed by Professor Rajagopal to Andrea Bonito, Diane Guignard and me.
- It is a model for the flow of **slow incompressible** fluids in a deformable porous solid, but it is **different** from the classical Biot model.
- The model for the solid's displacement is introduced and studied in "An implicit constitutive relation for describing the **small strain response** of porous elastic solids whose material moduli are dependent on the density", by Rajagopal, in Mathematics and Mechanics of Solids, 2021.
- This dependence has been **linearized**, but the equations of the model are **nonlinear**.
- Since the flow is **slow**, the motion of the fluid is governed by **Stokes system**.
- The flow and solid are **coupled by a reaction** term between the velocity of the solid and the velocity of the fluid.

Constitutive equation for the solid

- \mathbf{T}_s : symmetric Cauchy stress tensor of solid, \mathbf{u}_s : solid's displacement
 $\boldsymbol{\varepsilon}_s$: symmetric gradient tensor of \mathbf{u}_s , $\boldsymbol{\varepsilon}_s = \frac{1}{2}(\nabla \mathbf{u}_s + (\nabla \mathbf{u}_s)^T)$
- $\text{tr}(\mathbf{T}_s)$: trace of \mathbf{T}_s , $\text{tr}(\mathbf{T}_s) = \sum_{i=1}^d (T_s)_{i,i}$
- d : dimension, here we work in 3-D, i.e., $d = 3$
- **Implicit** constitutive relation for \mathbf{T}_s :

$$\boldsymbol{\varepsilon}_s = E_{1s}(1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s))\mathbf{T}_s + E_{2s}(1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))\text{tr}(\mathbf{T}_s)\mathbf{I}. \quad (1)$$

The linearization is justified by **the assumption** :

$$\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1 \quad (2)$$

- $\|\cdot\|$: Frobenius norm
- Model applies to porous metals, bones, rocks, concrete, undergoing small deformations

Constitutive equation for the solid

- \mathbf{T}_s : symmetric Cauchy stress tensor of solid, \mathbf{u}_s : solid's displacement
 $\boldsymbol{\varepsilon}_s$: symmetric gradient tensor of \mathbf{u}_s , $\boldsymbol{\varepsilon}_s = \frac{1}{2}(\nabla \mathbf{u}_s + (\nabla \mathbf{u}_s)^T)$
- $\text{tr}(\mathbf{T}_s)$: trace of \mathbf{T}_s , $\text{tr}(\mathbf{T}_s) = \sum_{i=1}^d (T_s)_{i,i}$
- d : dimension, here we work in 3-D, i.e., $d = 3$
- **Implicit** constitutive relation for \mathbf{T}_s :

$$\boldsymbol{\varepsilon}_s = E_{1s}(1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s))\mathbf{T}_s + E_{2s}(1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))\text{tr}(\mathbf{T}_s)\mathbf{I}. \quad (1)$$

The linearization is justified by **the assumption** :

$$\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1 \quad (2)$$

- $\|\cdot\|$: Frobenius norm
- Model applies to porous metals, bones, rocks, concrete, undergoing small deformations

Constitutive equation for the solid-II

$$\boldsymbol{\varepsilon}_s = E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)) \mathbf{T}_s + E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}.$$

- The linearized material moduli are :

$$E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)) \text{ and } E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))$$

- They are related to a **generalized** Young's modulus and a **generalized** Poisson's ratio if we define

$$\frac{1 + \nu_g}{E_g} = E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)), \quad \frac{-\nu_g}{E_g} = E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))$$

- Where is the dependence on density ?

The balance of mass and $\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1$ imply

$$\varrho_R = \varrho_s (1 + \text{tr}(\boldsymbol{\varepsilon}_s))$$

- ϱ_R : reference density, ϱ_s : actual density of the solid

Constitutive equation for the solid-II

$$\boldsymbol{\varepsilon}_s = E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)) \mathbf{T}_s + E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}.$$

- The linearized material moduli are :

$$E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)) \text{ and } E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))$$

- They are related to a **generalized** Young's modulus and a **generalized** Poisson's ratio if we define

$$\frac{1 + \nu_g}{E_g} = E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)), \quad \frac{-\nu_g}{E_g} = E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s))$$

- Where is the dependence on density ?

The balance of mass and $\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1$ imply

$$\varrho_R = \varrho_s (1 + \text{tr}(\boldsymbol{\varepsilon}_s))$$

- ϱ_R : reference density, ϱ_s : actual density of the solid

Constitutive equation for the solid-III

$$\boldsymbol{\varepsilon}_s = E_{1s} (1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)) \mathbf{T}_s + E_{2s} (1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}.$$

- From relations of E_{1s} and E_{2s} with E_g and ν_g , we expect

$$E_{1s} > 0 \text{ and } E_{2s} < 0 \text{ therefore } E_{2s} = -|E_{2s}|$$

- Assumption :

The parameters λ_2 and λ_3 are small in absolute value

- $\lambda_2 = 0$ and $\lambda_3 = 0$ imply standard **linear elasticity**

$$\boldsymbol{\varepsilon}_s = E_{1s} \mathbf{T}_s - |E_{2s}| \text{tr}(\mathbf{T}_s) \mathbf{I}.$$

- Therefore the nonlinear model is a perturbation of a linear model.

Balance of linear momentum for the solid

- Assumption :

Acceleration of the solid $\partial_{tt}^2 \mathbf{u}_s$ is **negligible**

- Balance of linear momentum takes into account interaction with the fluid

$$\operatorname{div}(\mathbf{T}_s) + \alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) = \mathbf{0}, \quad (3)$$

- \mathbf{v}_f : velocity of fluid, $\partial_t \mathbf{u}_s$: velocity of solid

- **Interaction term :**

$$\alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s)$$

Equation of motion of the fluid

- p_f : fluid's pressure, $\mu_f > 0$: constant viscosity of fluid,
 $\varrho_f > 0$: constant density of fluid
- Flow equation of the fluid taking into account **interaction** with the solid :

$$\alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) - \mu_f \Delta \mathbf{v}_f + \nabla p_f = -\varrho_f \partial_t \mathbf{v}_f \quad (4)$$

- Conservation of mass :

$$\operatorname{div} \mathbf{v}_f = 0 \quad (5)$$

- (4)–(5) is a standard Stokes system + the interaction term

Preliminary summary of equations

$$\boldsymbol{\varepsilon}_s = E_{1s} \left(1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s) \right) \mathbf{T}_s - |E_{2s}| \left(1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s) \right) \text{tr}(\mathbf{T}_s) \mathbf{I}$$

$$\mathbf{div}(\mathbf{T}_s) + \alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) = \mathbf{0}$$

$$\alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) - \mu_f \Delta \mathbf{v}_f + \nabla p_f = -\varrho_f \partial_t \mathbf{v}_f$$

$$\text{div } \mathbf{v}_f = 0$$

- 13 equations in 13 unknowns
- plus suitable initial and boundary conditions
- We must include hypothesis (2) that permitted the linearization :

$$\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1$$

- It means that \mathbf{u}_s is small in $W^{1,\infty}$ in space and time

Preliminary summary of equations

$$\boldsymbol{\varepsilon}_s = E_{1s} \left(1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s)\right) \mathbf{T}_s - |E_{2s}| \left(1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s)\right) \text{tr}(\mathbf{T}_s) \mathbf{I}$$

$$\mathbf{div}(\mathbf{T}_s) + \alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) = \mathbf{0}$$

$$\alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) - \mu_f \Delta \mathbf{v}_f + \nabla p_f = -\varrho_f \partial_t \mathbf{v}_f$$

$$\text{div } \mathbf{v}_f = 0$$

- 13 equations in 13 unknowns
- plus suitable initial and boundary conditions
- We must include hypothesis (2) that permitted the linearization :

$$\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1$$

- It means that \mathbf{u}_s is small in $W^{1,\infty}$ in space and time

Truncation of the factors

- As it is, this system is unmanageable because the factors

$$1 + \lambda_2 \text{tr}(\varepsilon_s) \text{ and } 1 + \lambda_3 \text{tr}(\varepsilon_s)$$

can only be controlled by hypothesis (2) : $\|\varepsilon_s\| \leq \delta \ll 1$
but how can it be used ?

- One possibility is to truncate $\text{tr}(\varepsilon_s)$
- Recall the truncation operator T_k for real $k > 0$

$$T_k f = f \quad \text{if } |f| \leq k, \quad T_k f = k \text{sign}(f) \quad \text{if } |f| > k.$$

- Then $\|\varepsilon_s\| \leq \delta$ implies that $|\text{tr}(\varepsilon_s)| \leq \sqrt{3}\delta$ and $\text{tr}(\varepsilon_s) = T_{\sqrt{3}\delta} \text{tr}(\varepsilon_s)$
- Therefore we can use

$$\varepsilon_s = E_{1s} (1 + \lambda_2 T_{\sqrt{3}\delta} \text{tr}(\varepsilon_s)) \mathbf{T}_s - |E_{2s}| (1 + \lambda_3 T_{\sqrt{3}\delta} \text{tr}(\varepsilon_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}$$

Truncation of the factors

- As it is, this system is unmanageable because the factors

$$1 + \lambda_2 \text{tr}(\boldsymbol{\varepsilon}_s) \text{ and } 1 + \lambda_3 \text{tr}(\boldsymbol{\varepsilon}_s)$$

can only be controlled by hypothesis (2) : $\|\boldsymbol{\varepsilon}_s\| \leq \delta \ll 1$
but how can it be used ?

- One possibility is to truncate $\text{tr}(\boldsymbol{\varepsilon}_s)$
- Recall the truncation operator T_k for real $k > 0$

$$T_k f = f \quad \text{if } |f| \leq k, \quad T_k f = k \text{sign}(f) \quad \text{if } |f| > k.$$

- Then $\|\boldsymbol{\varepsilon}_s\| \leq \delta$ implies that $|\text{tr}(\boldsymbol{\varepsilon}_s)| \leq \sqrt{3}\delta$ and $\text{tr}(\boldsymbol{\varepsilon}_s) = T_{\sqrt{3}\delta} \text{tr}(\boldsymbol{\varepsilon}_s)$
- Therefore we can use

$$\boldsymbol{\varepsilon}_s = E_{1s} (1 + \lambda_2 T_{\sqrt{3}\delta} \text{tr}(\boldsymbol{\varepsilon}_s)) \mathbf{T}_s - |E_{2s}| (1 + \lambda_3 T_{\sqrt{3}\delta} \text{tr}(\boldsymbol{\varepsilon}_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}$$

Inverting the displacement's constitutive relation

- To simplify denote $\sqrt{3}\delta$ by δ

$$\boldsymbol{\varepsilon}_s = E_{1s}(1 + \lambda_2 T_\delta \text{tr}(\boldsymbol{\varepsilon}_s)) \mathbf{T}_s - |E_{2s}|(1 + \lambda_3 T_\delta \text{tr}(\boldsymbol{\varepsilon}_s)) \text{tr}(\mathbf{T}_s) \mathbf{I}.$$

- Linearization has been done directly on the **implicit relation**.
But, mathematically the constitutive relation can be easily inverted and the inverted form is useful for mathematical analysis and discretization
- Take the **trace** of (1), recall $\text{tr}(\boldsymbol{\varepsilon}_s) = \text{div } \mathbf{u}_s$, $\text{tr}(\mathbf{I}) = d = 3$

$$\mathbf{T}_s = \frac{1}{E_{1s}(1 + \lambda_2 T_\delta \text{div } \mathbf{u}_s)} \left(\boldsymbol{\varepsilon}_s + |E_{2s}|(1 + \lambda_3 T_\delta \text{div } \mathbf{u}_s) \frac{\text{div } \mathbf{u}_s}{F(\mathbf{u}_s)} \mathbf{I} \right)$$

where

$$F(\mathbf{u}_s) = E_{1s}(1 + \lambda_2 T_\delta \text{div } \mathbf{u}_s) - 3|E_{2s}|(1 + \lambda_3 T_\delta \text{div } \mathbf{u}_s).$$

An attempt at analysis

THE LITTLE ANALYSIS WE COULD DO

Summary of equations

- Domain Ω , boundary $\partial\Omega$, time interval $(0, T)$
- Unknowns $\mathbf{u}_s, \mathbf{v}_f, p_f$ satisfying a.e. $t \in (0, T)$

$$\mathbf{T}_s = \frac{1}{E_{1s}(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s)} (\boldsymbol{\varepsilon}_s + |E_{2s}|(1 + \lambda_3 T_\delta \operatorname{div} \mathbf{u}_s) \frac{\operatorname{div} \mathbf{u}_s}{F(\mathbf{u}_s)} \mathbf{I})$$

$$F(\mathbf{u}_s) = E_{1s}(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s) - 3|E_{2s}|(1 + \lambda_3 T_\delta \operatorname{div} \mathbf{u}_s)$$

$$\operatorname{div}(\mathbf{T}_s) + \alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) = \mathbf{0}$$

$$\alpha(\mathbf{v}_f - \partial_t \mathbf{u}_s) - \mu_f \Delta \mathbf{v}_f + \nabla p_f = -\varrho_f \partial_t \mathbf{v}_f$$

$$\operatorname{div} \mathbf{v}_f = 0$$

- Boundary conditions (outrageously simplified in view of the analysis)

$$\mathbf{u}_s = \mathbf{0} \text{ on } \partial\Omega, \mathbf{v}_f = \mathbf{0} \text{ on } \partial\Omega$$

- Initial conditions

$$\mathbf{u}_s(0) = \mathbf{u}_{s,0}, \quad \mathbf{v}_f(0) = \mathbf{v}_{f,0}, \quad \operatorname{div} \mathbf{v}_{f,0} = 0, \quad \mathbf{u}_{s,0} = \mathbf{v}_{f,0} = \mathbf{0} \text{ on } \partial\Omega$$

Rough variational formulation

$$\begin{aligned} & \frac{1}{E_{1s}} \int_0^t \int_{\Omega} \left[\frac{1}{1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s} \boldsymbol{\varepsilon}(\mathbf{u}_s) : \boldsymbol{\varepsilon}(\mathbf{z}) \right. \\ & \quad \left. + \frac{|E_{2s}|(1 + \lambda_3 T_\delta \operatorname{div} \mathbf{u}_s)}{(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s)} \frac{\operatorname{div} \mathbf{u}_s}{F(\mathbf{u}_s)} \operatorname{div} \mathbf{z} \right] + \alpha \int_0^t \int_{\Omega} \partial_t \mathbf{u}_s \cdot \mathbf{z} \\ & = \alpha \int_0^t \int_{\Omega} \mathbf{v}_f \cdot \mathbf{z}, \end{aligned}$$

$$\begin{aligned} & \int_0^t \int_{\Omega} \varrho_f \partial_t \mathbf{v}_f \cdot \mathbf{w} + \mu_f \int_0^t \int_{\Omega} \nabla \mathbf{v}_f : \nabla \mathbf{w} + \alpha \int_0^t \int_{\Omega} \mathbf{v}_f \cdot \mathbf{w} \\ & \quad - \int_0^t \int_{\Omega} p_f \operatorname{div} \mathbf{w} = \alpha \int_0^t \int_{\Omega} \partial_t \mathbf{u}_s \cdot \mathbf{w}, \\ & \operatorname{div} \mathbf{v}_f = 0 \end{aligned}$$

- \mathbf{z} : test displacement in $L^2(0, T; H_0^1(\Omega)^3)$,
 \mathbf{w} : test velocity in $L^2(0, T; H_0^1(\Omega)^3)$

A little good news

ASSUMPTION ON THE PARAMETERS

$$E_{1s} - 3|E_{2s}| > 0$$

- and suppose that δ (and/or λ_2, λ_3) sufficiently small so that

$$0 < 1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s, \quad 0 < 1 + \lambda_3 T_\delta \operatorname{div} \mathbf{u}_s, \quad 0 < F(\mathbf{u}_s)$$

are bounded above and away from zero

recall $F(\mathbf{u}_s) = E_{1s}(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s) - 3|E_{2s}|(1 + \lambda_3 T_\delta \operatorname{div} \mathbf{u}_s)$

- Then the system is **unconditionally stable** in basic norms :

$$\|\mathbf{v}_f\|_{L^\infty(0,t;L^2(\Omega))}, \quad \|\mathbf{v}_f\|_{L^2(Q_t)} \text{ and } \|\nabla \mathbf{v}_f\|_{L^2(Q_t)} \leq C_1 \exp(C_2 t),$$

Q_t : time-space cylinder $\Omega \times]0, t[$

C_1 is small if $\|\mathbf{v}_{f,0}\|_{L^2(\Omega)}$ and $\|\mathbf{u}_{s,0}\|_{L^2(\Omega)}$ are small

C_2 depends on the parameters $\alpha, \mu_f, \varrho_f, E_{1s}, E_{2s}, \lambda_2, \lambda_3, \delta$

Stability estimates-II

- The displacement satisfies

$$\|\mathbf{u}_s\|_{L^\infty(0,t;L^2(\Omega))}, \quad \|\boldsymbol{\varepsilon}(\mathbf{u}_s)\|_{L^2(Q_t)}, \quad \|\operatorname{div} \mathbf{u}_s\|_{L^2(Q_t)}$$

and $\|\partial_t \mathbf{u}_s\|_{L^2(0,t;H^{-1}(\Omega))} \leq C_3 \|\mathbf{v}_f\|_{L^2(Q_t)} + C_4$

C_3 depends on the parameters

C_4 is small if $\|\mathbf{u}_{s,0}\|_{L^2(\Omega)}$ is small

- Similar bounds hold for the velocity plus pressure and for the pressure itself

$$\|\partial_t \mathbf{v}_f + \frac{1}{\varrho_f} \nabla p_f\|_{L^2(0,t;H^{-1}(\Omega))}, \quad \|p_f\|_{W^{-1,\infty}(0,t;L_0^2(\Omega))}$$

Very bas news

The system has neither compactness nor monotony

- No compactness : because of the term

$$\int_0^t \int_{\Omega} \frac{1}{1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s} \boldsymbol{\varepsilon}(\mathbf{u}_s) : \boldsymbol{\varepsilon}(\mathbf{z})$$

weak convergence of $\boldsymbol{\varepsilon}(\mathbf{u}_s)$ in $L^2(Q_t)$ and weak convergence of $\frac{1}{1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_s}$ in $L^\infty(Q_t)$ does not imply convergence of the product to the product of the limits

- No monotony : there is no reason why

$$\int_0^t \int_{\Omega} \left[\frac{1}{1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_1} \boldsymbol{\varepsilon}(\mathbf{u}_1) - \frac{1}{1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_2} \boldsymbol{\varepsilon}(\mathbf{u}_2) \right] : \boldsymbol{\varepsilon}(\mathbf{u}_1 - \mathbf{u}_2) > 0$$

An attempt with perturbation

- The fully linear problem is well-posed

$$\begin{aligned} \frac{1}{E_{1s}} \int_0^t \int_{\Omega} \left[\boldsymbol{\varepsilon}(\mathbf{u}_s) : \boldsymbol{\varepsilon}(\mathbf{z}) + \frac{|E_{2s}|}{E_{1s} - 3|E_{2s}|} \operatorname{div} \mathbf{u}_s \operatorname{div} \mathbf{z} \right] + \alpha \int_0^t \int_{\Omega} \partial_t \mathbf{u}_s \cdot \mathbf{z} \\ = \alpha \int_0^t \int_{\Omega} \mathbf{v}_f \cdot \mathbf{z}, \end{aligned}$$

$$\begin{aligned} \int_0^t \int_{\Omega} \varrho_f \partial_t \mathbf{v}_f \cdot \mathbf{w} + \mu_f \int_0^t \int_{\Omega} \nabla \mathbf{v}_f : \nabla \mathbf{w} + \alpha \int_0^t \int_{\Omega} \mathbf{v}_f \cdot \mathbf{w} \\ - \int_0^t \int_{\Omega} p_f \operatorname{div} \mathbf{w} = \alpha \int_0^t \int_{\Omega} \partial_t \mathbf{u}_s \cdot \mathbf{w}, \\ \operatorname{div} \mathbf{v}_f = 0 \end{aligned}$$

- We hope that a small perturbation has also a solution

General idea of perturbation

- Let $G^s(\lambda_2, \lambda_3, \mathbf{u}_s, \mathbf{v}_f)$ be the operator for the solid's displacement
let $G^f(\mathbf{u}_s, \mathbf{v}_f, p_f)$ be the operator for the flow
let $\mathcal{F}(\lambda_2, \lambda_3, \mathbf{u}_s, \mathbf{v}_f, p_f)$ be the operator for the nonlinear system
including the initial conditions :

$$\mathcal{F}(\lambda_2, \lambda_3, \mathbf{u}_s, \mathbf{v}_f, p_f) :=$$

$$(G^s(\lambda_2, \lambda_3, \mathbf{u}_s, \mathbf{v}_f), G^f(\mathbf{u}_s, \mathbf{v}_f, p_f), \mathbf{u}_s(0) - \mathbf{u}_{s,0}, \mathbf{v}_f(0) - \mathbf{v}_{f,0})$$

- The nonlinear system reads

$$\mathcal{F}(\lambda_2, \lambda_3, \mathbf{u}_s, \mathbf{v}_f, p_f) = (\mathbf{0}, \mathbf{0}, \mathbf{0}, \mathbf{0}).$$

- The fully linear system corresponds to $\lambda_2 = \lambda_3 = 0$
It has a unique solution, say $\mathbf{u}_{\text{lin}}, \mathbf{v}_{\text{lin}}, p_{\text{lin}}$:

$$\mathcal{F}(0, 0, \mathbf{u}_{\text{lin}}, \mathbf{v}_{\text{lin}}, p_{\text{lin}}) = (\mathbf{0}, \mathbf{0}, \mathbf{0}, \mathbf{0}).$$

General idea of perturbation-II

- Set $\omega = (\mathbf{u}, \mathbf{v}, p)$ and $\omega_{\text{lin}} = (\mathbf{u}_{\text{lin}}, \mathbf{v}_{\text{lin}}, p_{\text{lin}})$
Suppose $\mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})$ is differentiable with respect to ω
Let $D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})$ be the derivative
- If $D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})$ is **invertible**, then we can define the auxiliary function

$$\mathcal{H}(\lambda_2, \lambda_3, \omega) = \omega - [D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})]^{-1} \mathcal{F}(\lambda_2, \lambda_3, \omega)$$

and the fixed points of \mathcal{H} are the zeros of $\mathcal{F}(\lambda_2, \lambda_3, \omega)$

Computing the inverse of the derivative

- Three steps
 - ① Compute $D_{\omega}\mathcal{F}(0, 0, \omega_{\text{lin}})$
 - ② Compare with $D_{\omega}\mathcal{F}(\lambda_1, \lambda_2, \omega_{\text{lin}})$
 - ③ Deduce the inverse if the difference is less than one
- Start with the linear operator $\mathcal{F}(0, 0, \omega)$
Spaces : argument ω in \mathcal{X} and values in \mathcal{Y}
- Pick an increment $\theta = (\theta_u, \theta_v, \theta_p)$ in \mathcal{X}
Since $\mathcal{F}(0, 0, \omega)$ is linear, $D_{\omega}\mathcal{F}(0, 0, \omega)\theta$ has a simple expression
- And computing the inverse $[D_{\omega}\mathcal{F}(0, 0, \omega)]^{-1}$ amounts to solve for any set of values (g_u, g_v, a, b) in \mathcal{Y} the system : Find $\theta \in \mathcal{X}$

$$D_{\omega}\mathcal{F}(0, 0, \omega)\theta = (g_u, g_v, a, b)$$

Computing the inverse of the derivative

- Three steps
 - ① Compute $D_{\omega}\mathcal{F}(0, 0, \omega_{\text{lin}})$
 - ② Compare with $D_{\omega}\mathcal{F}(\lambda_1, \lambda_2, \omega_{\text{lin}})$
 - ③ Deduce the inverse if the difference is less than one
- Start with the linear operator $\mathcal{F}(0, 0, \omega)$
Spaces : argument ω in \mathcal{X} and values in \mathcal{Y}
- Pick an increment $\theta = (\theta_u, \theta_v, \theta_p)$ in \mathcal{X}
Since $\mathcal{F}(0, 0, \omega)$ is linear, $D_{\omega}\mathcal{F}(0, 0, \omega)\theta$ has a simple expression
- And computing the inverse $[D_{\omega}\mathcal{F}(0, 0, \omega)]^{-1}$ amounts to solve for any set of values $(\mathbf{g}_u, \mathbf{g}_v, \mathbf{a}, \mathbf{b})$ in \mathcal{Y} the system : Find $\theta \in \mathcal{X}$

$$D_{\omega}\mathcal{F}(0, 0, \omega)\theta = (\mathbf{g}_u, \mathbf{g}_v, \mathbf{a}, \mathbf{b})$$

Computing the inverse of the derivative-II

- Compute $D_{\omega}\mathcal{F}(\lambda_1, \lambda_2, \omega_{\text{lin}})\theta$
- All terms are good except

$$-\frac{\lambda_2}{E_{1s}} \frac{\boldsymbol{\varepsilon}(\mathbf{u}_{\text{lin}}) : \boldsymbol{\varepsilon}(\mathbf{z})}{(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_{\text{lin}})^2} s(\operatorname{div} \mathbf{u}_{\text{lin}}) \operatorname{div} \theta_u,$$

here $s(\cdot)$ comes from differentiating the truncation :

$s(f) = 1$ if $|f| \leq \delta$ and $s(f) = 0$ if $|f| > \delta$

- It can be controlled if we assume

$$\|\boldsymbol{\varepsilon}(\mathbf{u}_{\text{lin}})\|_{L^\infty(Q_T)} \leq \delta$$

- Then

$$\|D_{\omega}\mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}}) - D_{\omega}\mathcal{F}(0, 0, \omega_{\text{lin}})\| \leq \frac{\delta}{E_{1s}} A_1$$

where A_1 is small if λ_2 and λ_3 are small.

Computing the inverse of the derivative-II

- Compute $D_{\omega}\mathcal{F}(\lambda_1, \lambda_2, \omega_{\text{lin}})\theta$
- All terms are good except

$$-\frac{\lambda_2}{E_{1s}} \frac{\boldsymbol{\varepsilon}(\mathbf{u}_{\text{lin}}) : \boldsymbol{\varepsilon}(\mathbf{z})}{(1 + \lambda_2 T_\delta \operatorname{div} \mathbf{u}_{\text{lin}})^2} s(\operatorname{div} \mathbf{u}_{\text{lin}}) \operatorname{div} \theta_u,$$

here $s(\cdot)$ comes from differentiating the truncation :

$s(f) = 1$ if $|f| \leq \delta$ and $s(f) = 0$ if $|f| > \delta$

- It can be controlled if we **assume**

$$\|\boldsymbol{\varepsilon}(\mathbf{u}_{\text{lin}})\|_{L^\infty(Q_T)} \leq \delta$$

- Then

$$\|D_{\omega}\mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}}) - D_{\omega}\mathcal{F}(0, 0, \omega_{\text{lin}})\| \leq \frac{\delta}{E_{1s}} A_1$$

where A_1 is small if λ_2 and λ_3 are small.

Finding the fixed points of $\mathcal{H}(\lambda_2, \lambda_3, \omega)$

- Recall

$$\mathcal{H}(\lambda_2, \lambda_3, \omega) = \omega - [D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})]^{-1} \mathcal{F}(\lambda_2, \lambda_3, \omega)$$

- Standard technique : construct a sequence ω_k with

$$\omega_{k+1} = \omega_k - [D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}})]^{-1} \mathcal{F}(\lambda_2, \lambda_3, \omega_k)$$

with obvious starting function $\omega_0 = \omega_{\text{lin}}$

- If it converges, the limit solves the problem

There is no free lunch

- To show convergence, consider two consecutive iterates ω_k, ω_{k+1}
set $\theta = \omega_{k+1} - \omega_k$
- As part of the calculation, we have to estimate

$$\int_0^1 (D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_{\text{lin}}) - D_\omega \mathcal{F}(\lambda_2, \lambda_3, \omega_k + \tau \theta)) \theta \, d\tau$$

for this we assume that

$$\|\varepsilon(\mathbf{u}_k)\|_{L^\infty(Q_T)} \leq \delta$$

this is the weak point of the analysis because it is very restrictive

- If it holds then it gives existence.

FINITE-ELEMENT DISCRETIZATION

General Numerical Scheme

DISCRETIZATION IN SPACE

- Assume domain is Lipschitz polyhedron, h : meshsize
 \mathcal{T}_h shape-regular mesh of $\bar{\Omega}$
- Discrete space for \mathbf{u}_s : $\mathbf{U}_h \subset H_0^1(\Omega)^3$, eg. piecewise $(\mathbb{P}_2)^3$
- Pair of discrete spaces for \mathbf{v}_f, p^f : $\mathbf{X}_h \subset H_0^1(\Omega)^3$, $Q_h \subset L_0^2(\Omega)$
stable for the divergence, eg. Hood–Taylor $(\mathbb{P}_2)^3 - \mathbb{P}_1$
- Approximation of the divergence-free functions

$$\mathbf{V}_h = \{ \mathbf{v}_h \in \mathbf{X}_h ; \int_{\Omega} q_h \operatorname{div} \mathbf{v}_h = 0, \forall q_h \in Q_h \}$$

- Π_h : interpolation operator from $H_0^1(\Omega)^3$ into \mathbf{X}_h or \mathbf{U}_h

DISCRETIZATION IN TIME

- Choose $N > 1$, set time step : $\Delta t = \frac{T}{N}$, discrete times : $t_n = n\Delta t$
- Use backward Euler for the time derivative, implicit but time-lagging for the nonlinear factors

General Numerical Scheme

DISCRETIZATION IN SPACE

- Assume domain is Lipschitz polyhedron, h : meshsize
 \mathcal{T}_h shape-regular mesh of $\bar{\Omega}$
- Discrete space for \mathbf{u}_s : $\mathbf{U}_h \subset H_0^1(\Omega)^3$, eg. piecewise $(\mathbb{P}_2)^3$
- Pair of discrete spaces for \mathbf{v}_f, p^f : $\mathbf{X}_h \subset H_0^1(\Omega)^3$, $Q_h \subset L_0^2(\Omega)$
stable for the divergence, eg. Hood–Taylor $(\mathbb{P}_2)^3 - \mathbb{P}_1$
- Approximation of the divergence-free functions

$$\mathbf{V}_h = \{ \mathbf{v}_h \in \mathbf{X}_h ; \int_{\Omega} q_h \operatorname{div} \mathbf{v}_h = 0, \forall q_h \in Q_h \}$$

- Π_h : interpolation operator from $H_0^1(\Omega)^3$ into \mathbf{X}_h or \mathbf{U}_h

DISCRETIZATION IN TIME

- Choose $N > 1$, set time step : $\Delta t = \frac{T}{N}$, discrete times : $t_n = n\Delta t$
- Use backward Euler for the time derivative, implicit but time-lagging for the nonlinear factors

The numerical scheme

- Starting from

$$\mathbf{u}_h^0 = \Pi_h \mathbf{u}_{0,s}, \quad \mathbf{v}_h^0 = \Pi_h \mathbf{v}_{0,f},$$

- then given $\mathbf{u}_h^{n-1} \in \mathbf{U}_h$ and $\mathbf{v}_h^{n-1} \in \mathbf{V}_h$ find $\mathbf{u}_h^n \in \mathbf{U}_h$, $\mathbf{v}_h^n \in \mathbf{V}_h$ and $p_h^n \in Q_h$ satisfying for all $\mathbf{z}_h \in \mathbf{U}_h$,

$$\begin{aligned} & \frac{\alpha}{\Delta t} \int_{\Omega} (\mathbf{u}_h^n - \mathbf{u}_h^{n-1}) \cdot \mathbf{z}_h + \frac{1}{E_{1s}} \int_{\Omega} \frac{1}{1 + \lambda_2 T_{\delta} \operatorname{div} \mathbf{u}_h^{n-1}} \boldsymbol{\varepsilon}(\mathbf{u}_h^n) : \boldsymbol{\varepsilon}(\mathbf{z}_h) \\ & + \frac{|E_{2s}|}{E_{1s}} \int_{\Omega} \frac{1 + \lambda_3 T_{\delta} \operatorname{div} \mathbf{u}_h^{n-1}}{(1 + \lambda_2 T_{\delta} \operatorname{div} \mathbf{u}_h^{n-1})} \frac{1}{F(\mathbf{u}_h^{n-1})} (\operatorname{div} \mathbf{u}_h^n) (\operatorname{div} \mathbf{z}_h) \\ & = \alpha \int_{\Omega} \mathbf{v}_h^n \cdot \mathbf{z}_h, \end{aligned}$$

where $F(\mathbf{u}_h^{n-1}) = E_{1s} - 3|E_{2s}| + (E_{1s}\lambda_2 - 3|E_{2s}|\lambda_3)T_{\delta} \operatorname{div} \mathbf{u}_h^{n-1}$

The numerical scheme-II

- and for all $\mathbf{w}_h \in \mathbf{X}_h$,

$$\begin{aligned} & \frac{\varrho_f}{\Delta t} \int_{\Omega} (\mathbf{v}_h^n - \mathbf{v}_h^{n-1}) \cdot \mathbf{w}_h - \int_{\Omega} p_h^n \operatorname{div} \mathbf{w}_h + \mu_f \int_{\Omega} \nabla \mathbf{v}_h^n : \nabla \mathbf{w}_h \\ & + \alpha \int_{\Omega} \mathbf{v}_h^n \cdot \mathbf{w}_h = \frac{\alpha}{\Delta t} \int_{\Omega} (\mathbf{u}_h^n - \mathbf{u}_h^{n-1}) \cdot \mathbf{w}_h \end{aligned}$$

- At each step n , this coupled **linear** system in finite dimension has a **unique** solution

Stability independent of the exact solution

- Assumptions

- ① Stability and approximation property of Π_h , $\forall \mathbf{u} \in H_0^1(\Omega)^3$

$$\|\nabla \Pi_h \mathbf{u}\|_{L^2(\Omega)} \leq C \|\nabla \mathbf{u}\|_{L^2(\Omega)} \text{ and } \|\mathbf{u} - \Pi_h \mathbf{u}\|_{L^2(\Omega)} \leq Ch \|\nabla \mathbf{u}\|_{L^2(\Omega)}$$

used for the initial data and for estimating in H^{-1} the discrete time derivative of \mathbf{u}_h

- ② Relation between the steps

$$h^2 \leq \Delta t$$

also used for estimating in H^{-1} the discrete time derivative of \mathbf{u}_h

- ③ Restriction on the time step : Δt sufficiently small

$$\Delta t \leq \tau, \quad \tau \text{ fixed, depending on the parameters}$$

used in applying discrete Gronwall's lemma

Stability independent of the exact solution-II

- Then

$$\|\mathbf{v}_h^n\|_{L^2(\Omega)}^2, \sum_{i=1}^{n-1} \|\mathbf{v}_h^i - \mathbf{v}_h^{i-1}\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\nabla \mathbf{v}_h^i\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\mathbf{v}_h^i\|_{L^2(\Omega)}^2 \\ \leq C_1 \exp(C_2 t_n)$$

$$\|\mathbf{u}_h^n\|_{L^2(\Omega)}^2, \sum_{i=1}^n \|\mathbf{u}_h^i - \mathbf{u}_h^{i-1}\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\boldsymbol{\varepsilon}(\mathbf{u}_h^i)\|_{L^2(\Omega)}^2, \\ \sum_{i=1}^n \Delta t \|\operatorname{div} \mathbf{u}_h^i\|_{L^2(\Omega)}^2 \leq C_3 \exp(C_2 t_n)$$

- Similar estimate for $\|p_h\|_{W^{-1,\infty}(0,T;L_0^2(\Omega))}$

A priori error estimates – degree one in space

- Errors

$$\mathbf{e}_u^n := \Pi_h \mathbf{u}(t_n) - \mathbf{u}_h^n, \quad \mathbf{e}_v^n := \Pi_h \mathbf{v}(t_n) - \mathbf{v}_h^n$$

- If the exact solution is sufficiently smooth but **not necessarily small**

$$\begin{aligned} & \|\mathbf{e}_v^n\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\nabla \mathbf{e}_v^i\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\mathbf{e}_v^i\|_{L^2(\Omega)}^2 \\ & \leq (h^2 + (\Delta t)^2) C_4 \exp(C_5 t_n) \end{aligned}$$

$$\begin{aligned} & \|\mathbf{e}_u^n\|_{L^2(\Omega)}^2, \sum_{i=1}^n \|\mathbf{e}_u^i - \mathbf{e}_u^{i-1}\|_{L^2(\Omega)}^2, \sum_{i=1}^n \Delta t \|\boldsymbol{\varepsilon}(\mathbf{e}_u^i)\|_{L^2(\Omega)}^2, \\ & \sum_{i=1}^n \Delta t \|\operatorname{div} \mathbf{e}_u^i\|_{L^2(\Omega)}^2 \leq (h^2 + (\Delta t)^2) C_6 \exp(C_7 t_n) \end{aligned}$$

- Similar estimate for $\|e_p\|_{W^{-1,\infty}(0,T;L_0^2(\Omega))}$

Numerical experiment in 2 – D

- Results using *deal.ii* and Paraview for visualization
- Domain : $\Omega = (0, 1)^2$, unit cube, final time : $T = 1$

$$\alpha = 1, \mu_f = 1, \varrho_f = 1, \lambda_2 = \lambda_3 = 0.1, E_{1s} = 1, E_{2s} = -0.2, \delta = 0.4$$

- Spaces $\mathbf{U}_h : \mathbb{Q}_2$, $\mathbf{X}_h : \mathbb{Q}_2$, $Q_h : \mathbb{Q}_1$
- Manufactured solution
time factor

$$\theta(t) = \theta_1(t) := \exp(-t) \quad \text{or} \quad \theta(t) = \theta_2(t) := \sin(3\pi t).$$

$$\mathbf{u}(t, \mathbf{x}) = \frac{\theta(t)}{100} \begin{pmatrix} \cos(2\pi x_1) \sin(2\pi x_2) \\ \sin(2\pi x_1) \cos(2\pi x_2) \end{pmatrix}$$

$$\mathbf{v}(t, \mathbf{x}) = \theta(t) \begin{pmatrix} \sin(2\pi x_1) \cos(2\pi x_2) \\ -\cos(2\pi x_1) \sin(2\pi x_2) \end{pmatrix}$$

$$p(\mathbf{x}, t) = \theta(t)(60x_1^2 x_2 - 20x_2^3 - 5)$$

force terms and non-homogeneous Dirichlet boundary conditions are added to the system

Numerical results—I

- $N = 20, 40, 80, 160, m = 5, 6, 7, \mathcal{T}_h : 2^{2m}$ square elements $h = \sqrt{2}(2^{-m})$

m	N	$\mathbf{e}_u^{H_0^1}$	$\mathbf{e}_u^{L^2}$	$\mathbf{e}_v^{H_0^1}$	$\mathbf{e}_v^{L^2}$
5	20	$6.0694 \cdot 10^{-5}$	$2.5565 \cdot 10^{-6}$	$5.8579 \cdot 10^{-3}$	$1.1499 \cdot 10^{-4}$
5	40	$5.9344 \cdot 10^{-5}$	$1.3452 \cdot 10^{-6}$	$5.8790 \cdot 10^{-3}$	$6.7737 \cdot 10^{-5}$
5	80	$5.9183 \cdot 10^{-5}$	$7.5595 \cdot 10^{-7}$	$5.9028 \cdot 10^{-3}$	$4.9307 \cdot 10^{-5}$
5	160	$5.9238 \cdot 10^{-5}$	$5.1058 \cdot 10^{-7}$	$5.9180 \cdot 10^{-3}$	$4.3989 \cdot 10^{-5}$
6	20	$2.3337 \cdot 10^{-5}$	$2.5496 \cdot 10^{-6}$	$1.7063 \cdot 10^{-3}$	$1.0966 \cdot 10^{-4}$
6	40	$1.7316 \cdot 10^{-5}$	$1.3086 \cdot 10^{-6}$	$1.5342 \cdot 10^{-3}$	$5.6185 \cdot 10^{-5}$
6	80	$1.5458 \cdot 10^{-5}$	$6.6689 \cdot 10^{-7}$	$1.4922 \cdot 10^{-3}$	$2.8774 \cdot 10^{-5}$
6	160	$1.4975 \cdot 10^{-5}$	$3.3824 \cdot 10^{-7}$	$1.4837 \cdot 10^{-3}$	$1.5162 \cdot 10^{-5}$
7	20	$1.8670 \cdot 10^{-5}$	$2.5505 \cdot 10^{-6}$	$9.7393 \cdot 10^{-4}$	$1.0965 \cdot 10^{-4}$
7	40	$9.9300 \cdot 10^{-6}$	$1.3091 \cdot 10^{-6}$	$5.8362 \cdot 10^{-4}$	$5.6058 \cdot 10^{-5}$
7	80	$5.9230 \cdot 10^{-6}$	$6.6644 \cdot 10^{-7}$	$4.3337 \cdot 10^{-4}$	$2.8421 \cdot 10^{-5}$
7	160	$4.3675 \cdot 10^{-6}$	$3.3601 \cdot 10^{-7}$	$3.8703 \cdot 10^{-4}$	$1.4363 \cdot 10^{-5}$

TABLE – Errors for the manufactured solution with $\theta = \theta_1$.

Numerical results-II

m	N	$\mathbf{e}_u^{H_0^1}$	$\mathbf{e}_u^{L^2}$	$\mathbf{e}_v^{H_0^1}$	$\mathbf{e}_v^{L^2}$
5	20	$1.5468 \cdot 10^{-3}$	$2.3046 \cdot 10^{-4}$	$8.6103 \cdot 10^{-2}$	$1.0423 \cdot 10^{-2}$
5	40	$7.9397 \cdot 10^{-4}$	$1.1828 \cdot 10^{-4}$	$4.3897 \cdot 10^{-2}$	$5.2890 \cdot 10^{-3}$
5	80	$4.0548 \cdot 10^{-4}$	$5.9907 \cdot 10^{-5}$	$2.2736 \cdot 10^{-2}$	$2.6595 \cdot 10^{-3}$
5	160	$2.1132 \cdot 10^{-4}$	$3.0172 \cdot 10^{-5}$	$1.2661 \cdot 10^{-2}$	$1.3342 \cdot 10^{-3}$
6	20	$1.5454 \cdot 10^{-3}$	$2.3044 \cdot 10^{-4}$	$8.5882 \cdot 10^{-2}$	$1.0421 \cdot 10^{-2}$
6	40	$7.9143 \cdot 10^{-4}$	$1.1826 \cdot 10^{-4}$	$4.3460 \cdot 10^{-2}$	$5.2872 \cdot 10^{-3}$
6	80	$4.0060 \cdot 10^{-4}$	$5.9882 \cdot 10^{-5}$	$2.1880 \cdot 10^{-2}$	$2.6575 \cdot 10^{-3}$
6	160	$2.0194 \cdot 10^{-4}$	$3.0145 \cdot 10^{-5}$	$1.1051 \cdot 10^{-2}$	$1.3319 \cdot 10^{-3}$
7	20	$1.5453 \cdot 10^{-3}$	$2.3044 \cdot 10^{-4}$	$8.5868 \cdot 10^{-2}$	$1.0421 \cdot 10^{-2}$
7	40	$7.9127 \cdot 10^{-4}$	$1.1826 \cdot 10^{-4}$	$4.3433 \cdot 10^{-2}$	$5.2871 \cdot 10^{-3}$
7	80	$4.0029 \cdot 10^{-4}$	$5.9880 \cdot 10^{-5}$	$2.1825 \cdot 10^{-2}$	$2.6574 \cdot 10^{-3}$
7	160	$2.0133 \cdot 10^{-4}$	$3.0144 \cdot 10^{-5}$	$1.0942 \cdot 10^{-2}$	$1.3318 \cdot 10^{-3}$

TABLE – Errors for the manufactured solution with $\theta = \theta_2$.

Numerical results-III

		$\theta = \theta_1$		$\theta = \theta_2$	
m	N	$\mathbf{e}_u^{H_0^1}$	rate	$\mathbf{e}_u^{H_0^1}$	rate
4	10	$2.2859 \cdot 10^{-4}$	—	$2.9561 \cdot 10^{-3}$	—
5	40	$5.9344 \cdot 10^{-5}$	1.946	$7.9397 \cdot 10^{-4}$	1.897
6	160	$1.4975 \cdot 10^{-5}$	1.987	$2.0194 \cdot 10^{-4}$	1.975

m	N	$\mathbf{e}_v^{H_0^1}$	rate	$\mathbf{e}_v^{H_0^1}$	rate
4	10	$2.2632 \cdot 10^{-2}$	—	$1.6862 \cdot 10^{-1}$	—
5	40	$5.8790 \cdot 10^{-3}$	1.945	$4.3897 \cdot 10^{-2}$	1.942
6	160	$1.4837 \cdot 10^{-3}$	1.986	$1.1051 \cdot 10^{-2}$	1.990

m	N	$e_p^{L^2}$	rate	$e_p^{L^2}$	rate
4	10	$9.0339 \cdot 10^{-3}$	—	$1.3004 \cdot 10^{-1}$	—
5	40	$2.3427 \cdot 10^{-3}$	1.946	$3.3711 \cdot 10^{-2}$	1.948
6	160	$5.9101 \cdot 10^{-4}$	1.987	$8.4744 \cdot 10^{-3}$	1.992

TABLE – Errors and convergence rate when $\Delta t = 12.8h^2$.

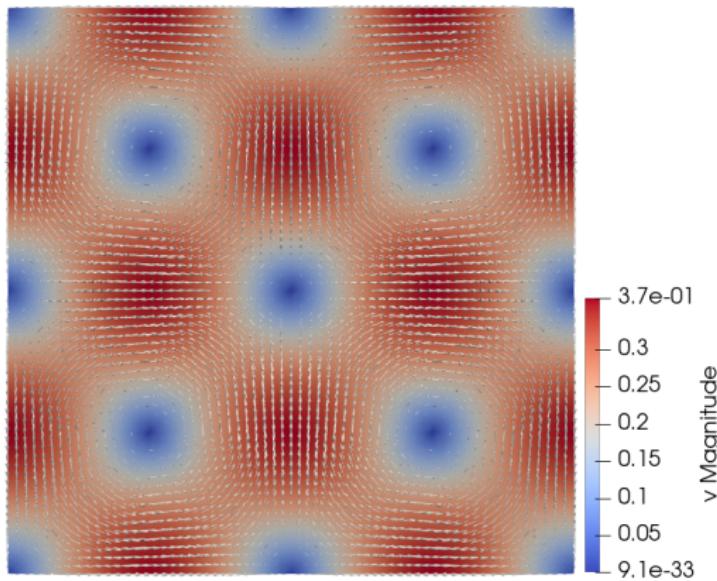
Numerical results–IV

m	3	4	5	6
$\mathbf{e}_u^{H^1_0}$	$9.5525 \cdot 10^{-4}$	$2.3769 \cdot 10^{-4}$	$5.9353 \cdot 10^{-5}$	$1.4838 \cdot 10^{-5}$
rate	—	2.00681	2.00168	2.00002
$\mathbf{e}_u^{L^2}$	$2.8425 \cdot 10^{-5}$	$3.5025 \cdot 10^{-6}$	$4.3565 \cdot 10^{-7}$	$7.2611 \cdot 10^{-8}$
rate	—	3.02067	3.00718	2.58490
$\mathbf{e}_v^{H^1_0}$	$9.4809 \cdot 10^{-2}$	$2.3725 \cdot 10^{-2}$	$5.9325 \cdot 10^{-3}$	$1.4833 \cdot 10^{-3}$
rate	—	1.99859	1.99971	1.99983
$\mathbf{e}_v^{L^2}$	$2.7696 \cdot 10^{-3}$	$3.4737 \cdot 10^{-4}$	$4.3459 \cdot 10^{-5}$	$5.7305 \cdot 10^{-6}$
rate	—	2.99514	2.99873	2.92292
$e_p^{L^2}$	$3.7580 \cdot 10^{-2}$	$9.3790 \cdot 10^{-3}$	$2.3439 \cdot 10^{-3}$	$5.8608 \cdot 10^{-4}$
rate	—	2.00247	2.00054	1.99971

TABLE – Errors and convergence rate for $\theta = \theta_1$ when $\Delta t = 0.001$.

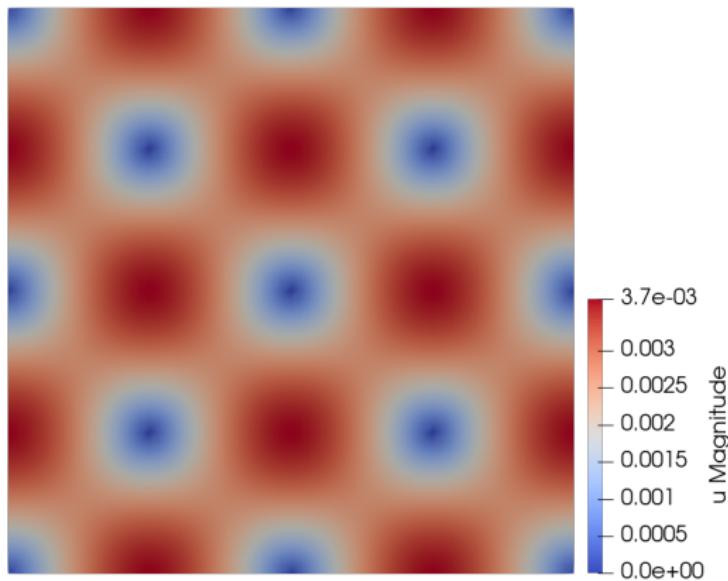
Fluid velocity, Plot

Fluid velocity



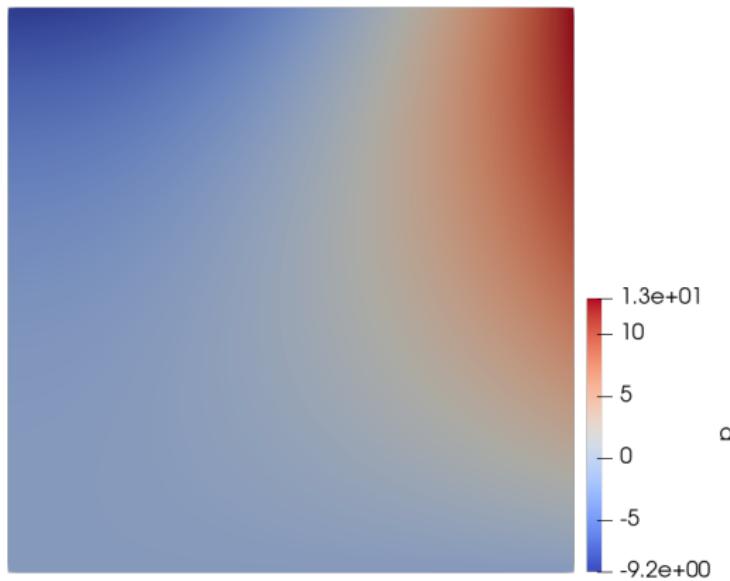
Displacement, Plot

Norm of solid displacement



Pressure, Plot

Pressure



Thanks

Happy Birthday Francisco and Manuel